Statistical fault detection and isolation for linear time-varying systems

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Overview Problem statement

Problem and approaches

FDI for LTV systems

- Relevant approach to FDI of NL systems (linearization along the actual or nominal trajectory)
- LTV systems more general than widely used LPV systems

Three main approaches

- Detection filter, game theoretic approach to filter design, unknown input decoupled filter, UIO, finite horizon fault detection filter Keviczky, Edelmayer, Chung-Speyer, Chen-Patton, Hou-Muller, Zhong-Ding, ...
- Adaptive observers, set-valued observers, time domain solutions to different $\mathcal{H}_-/\mathcal{H}_\infty$ problems Zhang-Xu, Rosa-Shamma-Athans, Li-Zhou, ...
- Parity-based fault estimation Zhong-Ding

Overview Problem statement

Model and assumptions

MIMO LTV system (\mathbb{H}_0)

$$\begin{array}{rclcrcrcrc} X_{k+1} & = & F_k \; X_k \; \; + \; \; G_k \; U_k \; \; + \; \; W_k \\ Y_k & = \; H_k \; X_k \; \; + \; \; J_k \; U_k \; \; + \; \; V_k \end{array}$$

 F_k, G_k, H_k, J_k : bounded TV matrices W_k, V_k : independent white Gaussian noises, TV cov. Q_k, R_k (H_k, F_k) observable & $(F_k, Q_k^{1/2})$ controllable, both uniformly

Additive faults (\mathbb{H}_1)

$$\begin{cases} X_{k+1} = F_k X_k + G_k U_k + W_k + \Psi_k \theta \\ Y_k = H_k X_k + J_k U_k + V_k \end{cases}$$

 θ : unknown fault vector Ψ_k : known TV fault profile

Overview Problem statement

Different fault cases

- Actuator bias: $U_k \rightarrow U_k + \theta$; then $\Psi_k = G_k$
- Actuator gain loss: U_k → (I − diag(θ))U_k; then Ψ_k = − G_k diag(U_k)
- Sensor faults: use a similar term $\Psi_k \theta$ on the output equation (not treated here)
- Different fault occurrence speeds:
 ex: step change Ψ_k(r) ≜ Ψ̃_k × 1_{k>r} (and θ constant)

A particular case

Ψ_k = δ_{r,k+1} I: investigated by Willsky-Jones, Gustafsson with *F_k* assumed exponentially stable

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Fault effect on the Kalman filter innovation

State prediction error and innovation - Fault free case

$$\begin{array}{rcl} \widetilde{X}_k & \stackrel{\Delta}{=} & X_k & - & \widehat{X}_{k|k-1} \\ \varepsilon_k & \stackrel{\Delta}{=} & Y_k & - & H_k \ \widehat{X}_{k|k-1} \end{array}$$

$$\begin{aligned} \widetilde{X}_{k+1}^{0} &= F_{k} \left(\mathbf{I} - K_{k} H_{k} \right) \widetilde{X}_{k}^{0} &- F_{k} K_{k} V_{k} + W_{k} \\ \varepsilon_{k}^{0} &= H_{k} \widetilde{X}_{k}^{0} + V_{k} \end{aligned}$$

State prediction error and innovation - Faulty case

$$\widetilde{X}_{k+1} = F_k \left(\mathbf{I} - K_k H_k \right) \widetilde{X}_k - F_k K_k V_k + W_k + \Psi_k \theta \varepsilon_k = H_k \widetilde{X}_k + V_k$$

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Introducing a matrix gain

$$\eta_{k} \stackrel{\Delta}{=} \widetilde{X}_{k} - \Gamma_{k} \theta$$

$$\Gamma_{k+1} \stackrel{\Delta}{=} F_{k} (\mathbf{I} - K_{k} H_{k}) \Gamma_{k} + \Psi_{k}, \ \Gamma_{0} \stackrel{\Delta}{=} 0$$

$$\eta_{k+1} = F_k \left(\mathbf{I} - K_k H_k \right) \eta_k - F_k K_k V_k + W_k$$

$$\eta_k = \widetilde{X}_k^0$$

Additive fault effect

$$\varepsilon_k = \varepsilon_k^0 + H_k \, \Gamma_k \, \theta$$

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Guaranteed properties of the recursive gain

- Γ_k depends on the fault gain Ψ_k , not on the fault vector θ .
- The matrix gain Γ_k computed from the bounded Ψ_k is bounded even when the system is not stable.
- The persistent excitation condition: $\sum_{k} \Gamma_{k}^{T} H_{k}^{T} \Sigma_{k}^{-1} H_{k} \Gamma_{k}$ strictly positive definite is satisfied even when the number of sensors is smaller than the number of faults.

Difference with the Willsky-Jones algorithm

Computations based on recursive formulas involving *F_k* (thus required to be stable)

Fault effect Detection algorithm Isolation algorithm

Known fault profile matrix

MLE of θ under \mathbb{H}_1

$$\begin{split} \mathbb{H}_{0} : \varepsilon_{k} \sim \mathcal{N}\left(0, \Sigma_{k}\right), & \mathbb{H}_{1} : \varepsilon_{k} \sim \mathcal{N}\left(H_{k} \Gamma_{k} \theta, \Sigma_{k}\right) \\ \widehat{\theta}_{k} = \arg\min_{\widetilde{\theta}} \sum_{j=1}^{k} (\varepsilon_{j} - H_{j} \Gamma_{j} \widetilde{\theta})^{T} \Sigma_{j}^{-1} (\varepsilon_{j} - H_{j} \Gamma_{j} \widetilde{\theta}) = C_{k}^{-1} d_{k} \\ C_{k} = C_{k-1} + \Gamma_{k}^{T} H_{k}^{T} \Sigma_{k}^{-1} H_{k} \Gamma_{k} \\ d_{k} = d_{k-1} + \Gamma_{k}^{T} H_{k}^{T} \Sigma_{k}^{-1} \varepsilon_{k} \end{split}$$

GLR test

$$I_{k} \triangleq 2 \ln \frac{p(\varepsilon_{1}, \ldots, \varepsilon_{k} \mid \theta = \widehat{\theta}_{k})}{p(\varepsilon_{1}, \ldots, \varepsilon_{k} \mid \theta = 0)} = d_{k}^{T} C_{k}^{-1} d_{k}$$

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Detection algorithm

Unknown jump fault onset time

Handling the transient behavior after a jump

$$\Psi_k(r) = \widetilde{\Psi}_k \times 1_{\{k \ge r\}} \Longrightarrow \Gamma_{k+1}(r) = F_k \left(\mathbf{I} - \mathcal{K}_k \mathcal{H}_k \right) \Gamma_k(r) + \Psi_k(r)$$

Full treatment of the transient

$$\widehat{\theta}_{k}(r) = C_{k}^{-1}(r) d_{k}(r)$$

$$I_{k} = \max_{1 \le r \le k} d_{k}^{T}(r) C_{k}^{-1}(r) d_{k}(r)$$

$$\widehat{r}_{k} = \arg \max_{1 \le r \le k} d_{k}^{T}(r) C_{k}^{-1}(r) d_{k}(r)$$

In practice

 $\Gamma_k(r), C_k(r), d_k(r)$ computed for $r \in \{k - w + 1, k - w + 2, ..., k\}$

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Locating non zero components

$$Z \stackrel{{\scriptstyle \triangle}}{=} \begin{bmatrix} \varepsilon_{\hat{r}+1} \\ \vdots \\ \varepsilon_{k} \end{bmatrix} \sim \mathcal{N} (M \theta, S)$$
$$M = \begin{bmatrix} H_{\hat{r}+1} \ \Gamma_{\hat{r}+1}(\hat{r}) \\ \vdots \\ H_{k} \ \Gamma_{k}(\hat{r}) \end{bmatrix}, \quad S = \operatorname{diag}(\Sigma_{\hat{r}+1}, \dots, \Sigma_{k})$$
$$\zeta \stackrel{{\scriptstyle \triangle}}{=} M^{T} S^{-1} Z, \quad \mathbb{F} \stackrel{{\scriptstyle \triangle}}{=} M^{T} S^{-1} M$$

 $\theta = \begin{bmatrix} \theta_a \\ \theta_b \end{bmatrix} - \theta_a = 0$ against $\theta_a \neq 0$, θ_b nuisance parameter

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Minmax test

$$I_a \stackrel{\Delta}{=} \zeta_a^{*T} \mathbb{F}_a^{*-1} \zeta_a^*$$

$$\zeta_a^* \stackrel{\Delta}{=} \zeta_a - \mathbb{F}_{ab} \mathbb{F}_{bb}^{-1} \zeta_b , \quad \mathbb{F}_a^* \stackrel{\Delta}{=} \mathbb{F}_{aa} - \mathbb{F}_{ab} \mathbb{F}_{bb}^{-1} \mathbb{F}_{ba}$$

 $I_a \sim \chi^2(\dim(\theta_a))$

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Leakage detection in gas transportation networks

Thanks to Paulo Lopes dos Santos et al., IEEE CST, Jan. 2011

Gas dynamics as a LPV model

Hyperbolic model linking edge pressure drop and mass flow

Discrete time LPV model

$$(X_{k+1} = (F_0 + F_p p_k) X_k + (G_0 + G_p p_k) U_k + K_k e_k$$

$$Y_k = (H_0 + H_p p_k) X_k + (J_0 + J_p p_k) U_k + e_k$$

 $U_k \in \mathbb{R}$: input mass flow, $Y_k \in \mathbb{R}$: output mass flow $X_k \in \mathbb{R}^2$: mass flow and pressure drop within the first section $p_k \in \mathbb{R}$: scheduling parameter (pressure pattern)

Simulated leakage

- Additive changes on G₀, G_p ∈ ℝ² (actuator gain loss) -Monitoring the first component
- Nominal values:
 - $G_0(1) = -7.8297e 4$ $G_p(1) = +3.8290e - 5$
- Changed values: $G_0(1) + 1.6e - 5$ Fault 1 $G_p(1) + 9.5e - 6$ Fault 2

Available data, simulated data

- U_k provided by P. Lopes dos Santos et al.
- Y_k simulated using the LPV model

A simulated example Numerical results Conclusion

Fault detection - Fault 1



Detection delay and onset time estimate - Fault 1



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Detection delay and onset time estimate - Fault 2





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Fault isolation with the minmax tests - Fault 1





Fault isolation with the minmax tests - Fault 2



FDI for LTV systems with TV additive faults

- Combining a recursive and stable filter that cancels out the fault dynamics and a GLR test
- Handling additive parametric faults with weaker assumptions than usual on the system stability and the number of required sensors
- Simulations confirm the stability of the proposed filter and suggest the relevance of the proposed approach
- Future investigations include numerical experiments on simulated and real cases to assess the quality of the full and simplified treatments of the transient