

Subspace-based modal identification

and monitoring of large structures:

The MODAL toolbox within Scilab

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Scilab and MODAL toolbox in

<http://www.scilab.org> <http://www.scilab.org/contrib>

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Modelling - Eigenstructure problem

$$\text{FE model: } \begin{cases} M \ddot{Z}(s) + C \dot{Z}(s) + K Z(s) = \nu(s) \\ Y(s) = L Z(s) \end{cases}$$

$$(M\mu^2 + C\mu + K) \Psi_\mu = 0, \quad \psi_\mu = L \Psi_\mu$$

$$\text{State space: } \begin{cases} X_{k+1} = F X_k + V_k \\ Y_k = H X_k \end{cases}$$

$$F \varphi_\lambda = \lambda \varphi_\lambda, \quad \phi_\lambda \triangleq H \varphi_\lambda$$

$$\text{Parameter: } \underbrace{e^{\delta\mu}}_{\text{modes}} = \lambda, \quad \underbrace{\psi_\mu = \phi_\lambda}_{\text{mode shapes}}; \quad \theta \triangleq \begin{pmatrix} \Lambda \\ \text{vec } \Phi \end{pmatrix}$$

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Framework: in-operation modal analysis

- **Excitation:** natural, not controlled,
not measured, nonstationary (e.g. turbulent)
 - **Output-only eigenstructure identification**
- **Merging data** from moving sensor pools
- **On-board detection** and **localization** of small damages.
 - **Avoid re-identification** prior to detection
 - **Avoid inverse problem solving** prior to damage localization

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Output-only covariance-based subspace identification

$$R_i \triangleq \underline{E(Y_k Y_{k-i}^T)}, \quad \mathcal{H} = \text{Hank}(R_i), \quad R_i = H F^i G$$

ok if stationary !

$$G \triangleq \underline{E(X_k Y_k^T)}, \quad \mathcal{O} \triangleq \begin{pmatrix} H \\ HF \\ HF^2 \\ \vdots \end{pmatrix}, \quad \mathcal{C} \triangleq (G \quad FG \quad F^2G \quad \dots)$$

$$\mathcal{H} = \mathcal{O} \mathcal{C}, \quad \mathcal{H} \longrightarrow \mathcal{O} \longrightarrow (H, F) \longrightarrow (\lambda, \varphi_\lambda)$$

$$\text{Implementation: } \hat{R}_i \triangleq \underline{1/n \sum_{k=1}^n Y_k Y_{k-i}^T}, \quad \hat{\mathcal{H}} = \text{Hank}(\hat{R}_i)$$

ok when nonstationary !

$$\text{SVD}(\hat{\mathcal{H}}) + \text{truncation} \longrightarrow \hat{\mathcal{O}} \longrightarrow (\hat{H}, \hat{F}) \longrightarrow (\hat{\lambda}, \hat{\varphi}_\lambda)$$

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Merging multiple measurements setups

$$\underbrace{\begin{bmatrix} Y_k^{(0,1)} \\ Y_k^{(1)} \end{bmatrix}}_{\text{Record 1}} \quad \underbrace{\begin{bmatrix} Y_k^{(0,2)} \\ Y_k^{(2)} \end{bmatrix}}_{\text{Record 2}} \quad \cdots \quad \underbrace{\begin{bmatrix} Y_k^{(0,J)} \\ Y_k^{(J)} \end{bmatrix}}_{\text{Record J}} \quad \begin{array}{l} \text{Fixed} \\ \text{Moving} \end{array}$$

$$R_i^{0,j} \triangleq E Y_k^{(0,j)} Y_{k-i}^{(0,j)T}, \quad R_i^j \triangleq E Y_k^{(j)} Y_{k-i}^{(0,j)T}, \quad G_j \triangleq E X_k^{(j)} Y_k^{(0,j)T}$$

$$R_i^{0,j} = H_0 F^i G_j, \quad R_i^j = H_j F^i G_j$$

Hint: right **renormalization** of the covariances

$$R_i^\pi \triangleq \begin{bmatrix} R_i^0 \\ R_i^1 \\ \vdots \\ R_i^J \end{bmatrix} = H F^i G, \quad H \triangleq \begin{bmatrix} H_0 \\ H_1 \\ \vdots \\ H_J \end{bmatrix}$$

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Eigenstructure monitoring

θ_0 : reference parameter, known (or identified)

Y_k : n -size sample of new measurements

System parameter characterization:

$\mathcal{H}_{p+1,q}$ and $\mathcal{O}_{p+1}(\theta)$ have the **same left kernel**.

$\exists U, \quad U^T U = I_s, \quad U^T \mathcal{O}_{p+1}(\theta_0) = 0; \quad \text{say } U(\theta_0)$

$\theta_0 \leftrightarrow (R_i^0)_i$ characterized by: $U^T(\theta_0) \hat{\mathcal{H}}_{p+1,q}^0 = 0$

Subspace-based residual for eigenstructure monitoring

$$\zeta_n(\theta_0) \triangleq \sqrt{n} \text{vec}(U^T(\theta_0) \hat{\mathcal{H}}_{p+1,q})$$

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Robustness to nonstationary excitation

The estimates are **consistent**.

Combination of:

- the key **factorization** property of the covariances,
- the **averaging** operation underlying covariance computation,

allows to cancel out nonstationarities in the excitation.

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The **residual** is asymptly **Gaussian** (local approach)

Mean **sensitivity** (Jacobian) $\mathcal{J}(\theta_0)$ and **covariance** $\Sigma(\theta_0)$

$$\zeta_n(\theta_0) \rightarrow \begin{cases} \mathcal{N}(\mathbf{0}, \Sigma(\theta_0)) & \text{under } P_{\theta_0} \\ \mathcal{N}(\mathcal{J}(\theta_0) \delta\theta, \Sigma(\theta_0)) & \text{under } P_{\theta_0 + \frac{\delta\theta}{\sqrt{n}}} \end{cases}$$

(GLR) χ^2 -test for modal monitoring

$$\zeta_n^T \Sigma^{-1} \mathcal{J} (\mathcal{J}^T \Sigma^{-1} \mathcal{J})^{-1} \mathcal{J}^T \Sigma^{-1} \zeta_n \geq h$$

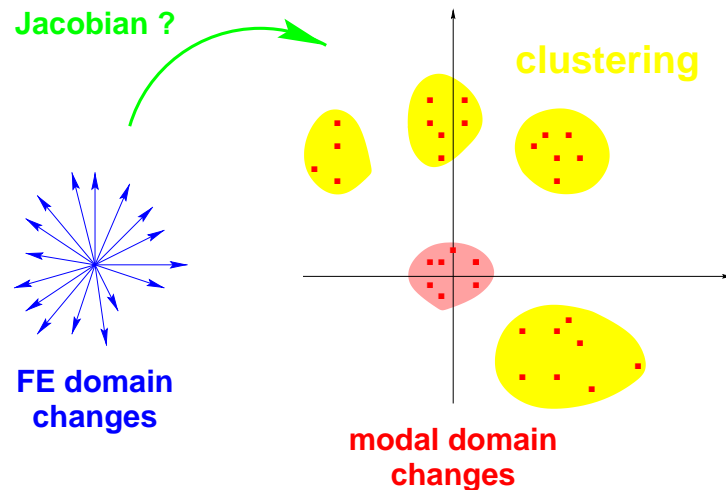
(GLR) **Directional** χ^2 -test for modal **diagnosis**

$$\zeta_n^T \Sigma^{-1} \mathcal{J}_i (\mathcal{J}_i^T \Sigma^{-1} \mathcal{J}_i)^{-1} \mathcal{J}_i^T \Sigma^{-1} \zeta_n \geq h$$

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On-board damage diagnostics

projecting changes and (local) sensitivity approach



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Some key features

- Processing:
Offline / Online (specified response time) / Very fast
- Huge model orders (several hundreds)
- Fixed order methods of no help
- AIC/BIC/... order selection criteria fail
- Model selection performed by heuristics, using certain properties of subspace methods

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The MODAL toolbox

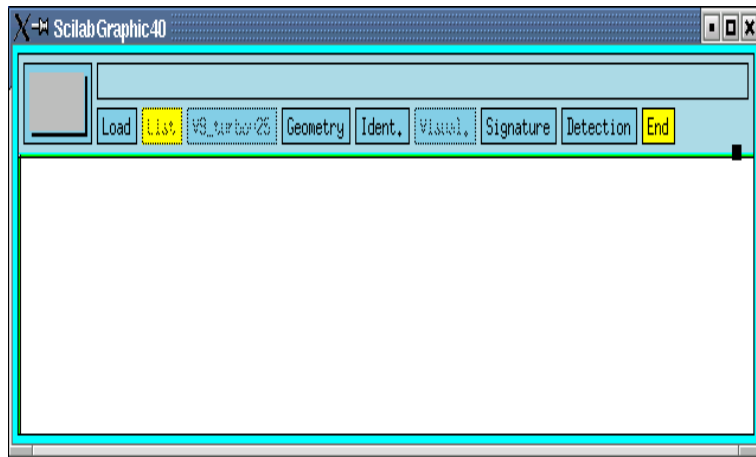
- Developed under Scilab (free)
- Completely driven by mouse/menu/parameter boxes
- Interactive graphical interface
- Automated and fully featured, easy to use
- Identification and damage detection/localization modules
- Based on covariance-driven subspace method
output-only and input-output versions
- Localization: interfaced with the FE Scilab toolbox

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Numerical results

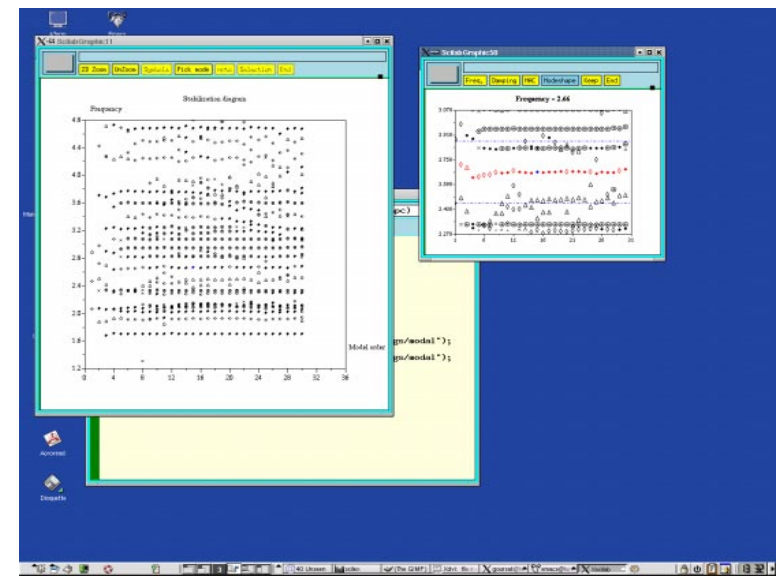
- Identification
 - Military aircraft (Dassault Aviation)
In-flight: decreasing fuel level → increasing frequencies
- Damage localization
 - Steelquake benchmark (COST F3)

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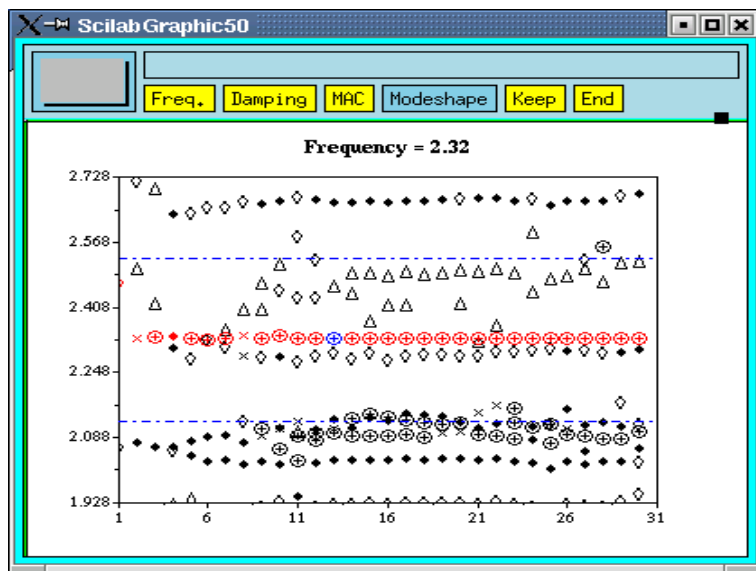
Main window

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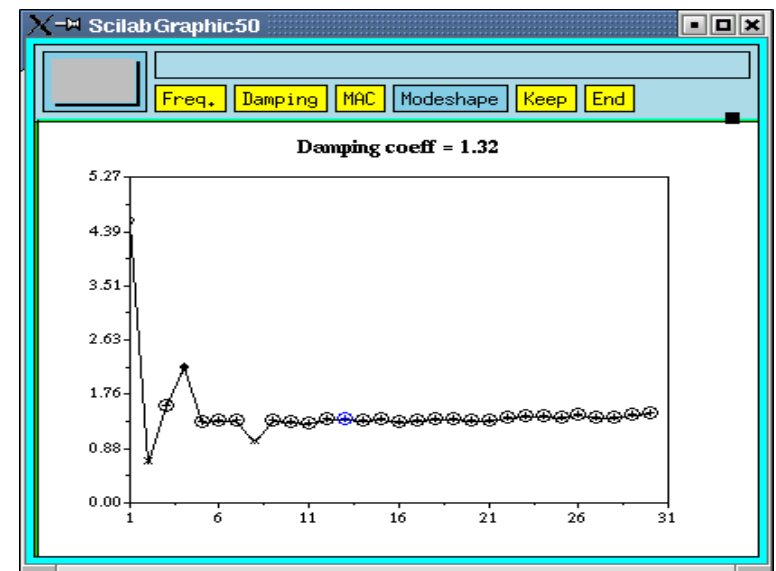
Identification window

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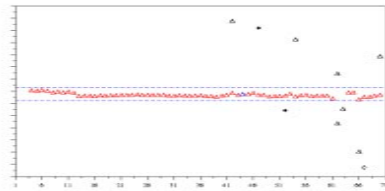
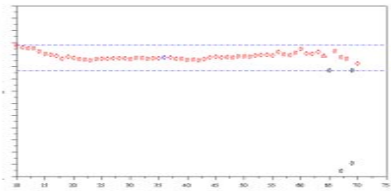
Stabilization diagram focussed on one frequency.

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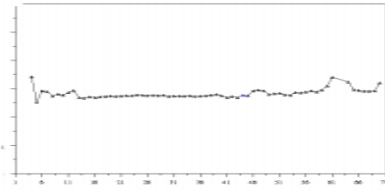
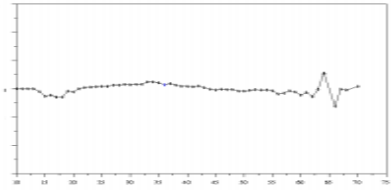


The corresponding damping values.

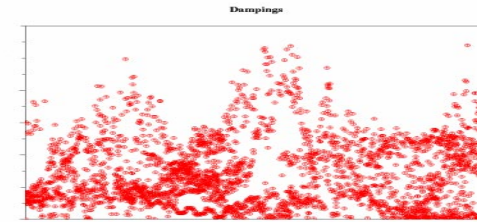
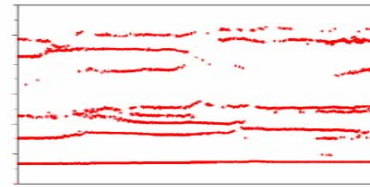
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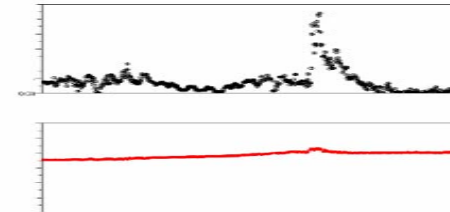
One eigenfrequency



The corresponding damping coefficient
Flight beginning (left), less fuel in tanks (right).

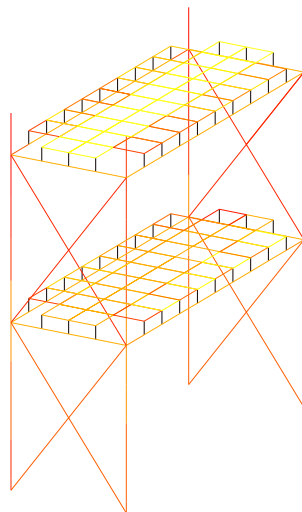


Automated identification: frequency (left) and damping (right) w.r.t. time.



Zoom on one mode: damping (top) and frequency (bottom).

Damage localization example - Steelquake benchmark



Under current investigation

- Handling **more** eigenfrequencies, hard **model selection** issue
 - new **huge** commercial aircrafts
- Designing a fast test for **monitoring damping** coefficients
 - aircrafts flight **flutter** issue
- Handling **environmental effects** (e.g. temperature)
 - civil engineering structures (**bridges**)

Identification (1) : offline

- Plot stabilization diagram for increasing orders
- Using the mouse, pick any mode for analysis
- Extract the corresponding alignment (frequency/damping/MAC)
- Simultaneous display of freq./damping/MAC w.r.t. order
- Plot and animate modeshapes
- Select and save good modes
- Save modal parameters for later use (identification/detection)

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Identification (2) : online

- Embedded and automated modal analysis
- Modes selection from histograms of frequency/damping/MAC
- Store “best” frequencies and dampings with their alignments
- Plot the evolution of the frequency and damping over time
- Pause for screening the extracted modes alignments
- Zoom on any mode for online monitoring

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Damage detection and localization

- **Offline:** Preprocessing, using safe data for estimating the reference model $(\theta_0, \mathcal{J}(\theta_0), \Sigma(\theta_0))$
- **Online:**
 - Monitoring: one index result per experiment
 - Localization: one index per FE plotted on the structure
 - Fast monitoring: one index result for each new sample
 - Displays: monitoring indexes on a time axis / localization results on the structure
 - Localization: plot the localized macro-failures

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